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# Fiber-Optic Temperature Sensor Based on Temperature-Dependent Refractive Index of Germanium-Silica Coating Stack

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We report on a novel fiber-optic temperature sensor based on the temperature-dependent refractive index of a germanium-silica (Ge-SiO<sub>2</sub>) coating stack. The relationship between the reflectivity and the temperature-dependent refractive index of the Ge-SiO<sub>2</sub> coating stack at 1550 nm is theoretically investigated. A reflection-type fiber-optic probe with high sensitivity and wide response range is designed and fabricated by physical vapor deposition. Experimental results show that the reflectivity is linearly dependent on temperature in the range of -30 to 130 °C, and the sensor exhibits high sensitivity and structural stability in the range of 50 to 500 K.

#### 1. Introduction

Owing to its fast response, fiber-optic temperature sensors with a wide dynamic range and telemetric optical fiber transmission network have widespread applications in remote or hazardous locations, such as underground mine and tunnel construction sites. (1,2) Owing to their invaluable advantages, various types of fiber-optic temperature sensors based on different materials and theories have been developed and fabricated. (3–5) GaAs, CdTe, and silicon-based sensors primarily rely on the temperature-dependent shift of the intrinsic absorption edge, whereas reflection-type optical fiber sensor systems require a grating panel. (6–11) Generally, fiber-optic temperature sensors using a crystal plate require precise positioning and special packaging technology. (12–15) In contrast, the process of

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coating thermo-optic films coated on the end face of an optical fiber offers a low-cost and promising technology. Semiconductor germanium (Ge) is an ideal thermo-optic sensing material as its thermal coefficient of refractive index and thermal stability are comparable to those of the best infrared coating materials. A fiber-optic temperature sensor based on the relationship between the temperature-dependent refractive index and the absorption of Ge films has been proposed recently.<sup>(16)</sup> In this article, we report on a reflection-type fiber-optic temperature sensor based on the temperature-dependent reflectivity of a Ge-SiO<sub>2</sub> coating stack, which exhibits high stability and simplicity in sensor structure.

## 2. Theoretical Model of Reflection-Type Sensor

The key feature of the reflection-type sensor is the germanium-silica (Ge-SiO<sub>2</sub>) stack coated on the end surface of an optical fiber, in which the Ge acts as a sensor layer and the SiO<sub>2</sub> as a protective layer, as shown in Fig. 1. On the basis of the optical admittance of the coating stacks, the intensity of the signal reflected back to the fiber core can be calculated and optimized by choosing a suitable thickness d of the film stack.

The light propagation characteristics of the fiber probe with the Ge-SiO $_2$  stack are studied by the equivalent conductance method. The characteristic matrices of the Ge layer and SiO $_2$  layer for calculating the reflection of the incident light at 1550 nm can be described by

$$\begin{bmatrix} B \\ C \end{bmatrix} = \left\{ \prod_{j=1}^{k} \begin{bmatrix} \cos \delta_{j} & \frac{i}{\eta_{j}} \sin \delta_{j} \\ i\eta_{j} \sin \delta_{j} & \cos \delta_{j} \end{bmatrix} \right\} \begin{bmatrix} 1 \\ \eta_{k+1} \end{bmatrix},$$

$$R = \left( \frac{\eta_{0}B - C}{\eta_{0}B + C} \right) \left( \frac{\eta_{0}B - C}{\eta_{0}B + C} \right)^{*},$$
(1)

where  $\delta_j = \frac{2\pi}{\lambda} n_j d_j \cos \theta_j$ ,  $\eta$  is the optical admittance related to the refractive index n and the incidence angle  $\theta$ , j is the layer numerical order, and k = 2.

In the optical fiber band at around 1550 nm, the extinction coefficient can be omitted and only the change in the refractive index of Ge with temperature is considered. From

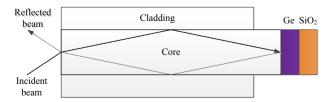


Fig. 1. (Color online) Schematic of the fiber probe of the reflection-type sensor.

the relationship between the semiconductor band gap energy  $E_{\rm g}$  and the temperature T, the refractive index of Ge can be expressed as<sup>(17)</sup>

$$n = \sqrt[4]{\frac{c}{E_{g}(0) - \gamma T^{2}/(T + \beta)}},$$
 (2)

where  $E_{\rm g}(0)$  is the forbidden gap at 0 K. In the range of 20–927 K,  $\gamma = 4.774 \times 10^{-4}$  eV/K,  $\beta = 235$  K,  $E_{\rm g}(0) = 0.75$  eV, and c = 224.6 eV. According to eqs. (1) and (2), the reflectivity of the stack can be expressed as a function of the thickness and thermal refractive index coefficient of the Ge-SiO<sub>2</sub> films. The reflectivity of the Ge coating as a function of film thickness at 273, 313, and 373 K is shown in Fig. 2. The reflectivity cyclically changes with the changes in the Ge film thickness, and the changes become more sensitive with increasing film thickness. The absorption coefficient of Ge (4.5969 ×  $10^{-5}$  at 1550 nm) is considered to be negligible only for sufficiently small film thickness. It is found that the difference in reflectivity for a 195 nm thickness is approximately 0.04 from 273 to 373 K. To minimize the absorption loss, the film thickness should be selected carefully and set in the first or second cycle.

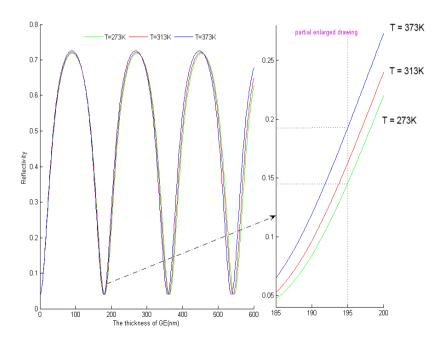


Fig. 2. (Color online) Reflectivity as a function of germanium film thickness.

## 3. Dependences of Measurement Range and Sensitivity on Thickness

Two important characteristic parameters, namely, measurement range and sensitivity, should be evaluated for the reflection-type fiber-optic temperature sensor. The measurement range is the difference between the maximum and minimum temperatures in an approximate linear range detected by the sensor. The reflectivity of the Ge film in a fiber core medium at the interface of the fiber core and Ge is calculated on the basis of Fresnel's formula. It is found that there is periodic variation in reflectivity with changing Ge film thickness. The Ge-SiO<sub>2</sub> film stack is considered here for two reasons: 1) sensitivity enhancement and 2) longer operating life.

The reflectivity of the  $Ge-SiO_2$  film stack is dependent on the film thickness, as shown in Fig. 3. Here, the approximate cyclical change is determined by the basic interference of the film, disregarding the change in absorptivity with temperature. In fact, the definition of absorptivity via an accurate mathematical expression is difficult. However, some approximation can be achieved by carefully selecting the change in absorptivity.

Figure 4 shows the reflectivity of a fiber detector with a single Ge layer over a temperature range from 30 to 550 K, which offers a wide measurement range. It is found that the reflectivity varies with temperature from 0.42 to 0.08. Different from the design described above, the silica layer changed the total reflectivity at the end surface of the fiber detector, as shown in Fig. 5. While maintaining the linearity with respect to the response to temperature change, there is no degradation in the measurement range of the fiber detector with the Ge-SiO<sub>2</sub> stack. In addition, the sensitivities are enhanced by decreasing the reflectivity to obtain a greater order of magnitude of the obtained signal. The final evaluation index of the fiber-optic temperature sensor in dBm is shown in Table 1.

Regarding the sensitivity of the films shown in Table 1, we found that the fiber sensor with the Ge-SiO<sub>2</sub> film stack probe exhibits higher sensitivity than that with only a single Ge film probe.

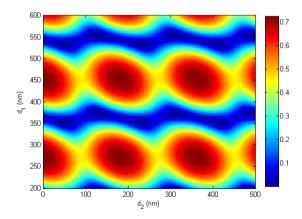


Fig. 3. (Color online) Reflectivity for various Ge (d<sub>1</sub>) and SiO<sub>2</sub> (d<sub>1</sub>) film thicknesses.

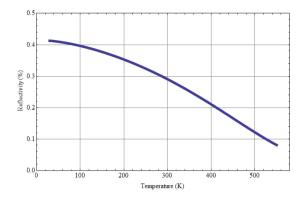


Fig. 4. (Color online) Reflectivity of a single Ge layer as a function of temperature.

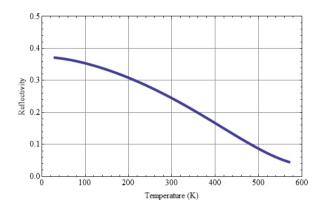


Fig. 5. (Color online) Reflectivity of the Ge-SiO<sub>2</sub> stack as a function of temperature.

Table 1 Evaluation index of the fiber-optic temperature sensor.

Type of sensor film	Difference in reflectivity (%)	Difference in signal (dBm)
Single Ge layer	34	26
Ge/SiO <sub>2</sub> stack	33	29

This is proved by data measurement in the temperature range of 30 to 130 °C, as shown in Fig. 6. Owing to cost consideration, the layer thicknesses of the Ge and  $SiO_2$  stack were 57.5 and 50 nm, respectively, and deposited on the end surface of the fiber by PVD with ion beam assistance (OTFC-900, Optorun, Japan). The reflectivity power of the Ge-SiO<sub>2</sub> film stack probe was approximately 4 dB for a temperature variation of 100 °C (-22.5 dBm at 30 °C; -26.49 dBm at 130 °C). Meanwhile, the reflectivity power

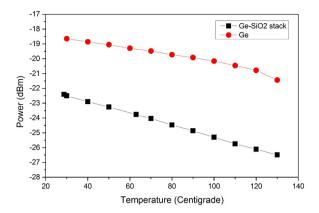


Fig. 6. (Color online) Experimental signal of fiber-optic temperature sensor.

of the fiber sensor with a single Ge film (57.5 nm) was 2.79 dB (-18.65 dBm at 30 °C; -21.44 dBm at 130 °C). The fiber sensor with the Ge-SiO<sub>2</sub> film stack probe exhibited 43% higher sensitivity than that with only a single Ge film in the range of -30 to 130 °C and 11% in a wider range of 50 to 500 K theoretically. The SiO<sub>2</sub> layer is capable of improving the sensitivity, in addition to protecting the Ge layer from oxidation and scratches.

### 4. Conclusions

We investigated theoretically and experimentally a novel fiber-optic temperature sensor based on the detection of reflection from Ge-SiO<sub>2</sub> film stacks. The Ge-SiO<sub>2</sub> stack was coated directly on the end surface of the optical fiber of the fiber optic probe by physical vapor deposition. We found that the fiber sensor with a Ge-SiO<sub>2</sub> film stack probe exhibited 11% higher sensitivity than that with only a single Ge film. Experimental results showed that the reflectivity exhibits a linear relationship with temperature in the range of -30 to 130 °C, and the sensor is capable of operating in the 50 to 500 K range. This study demonstrated the development of an optical fiber with a simple structure, high stability, and sensitivity.

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### References

- 1 G. Yilmaz and S. E. Karlik: Sens. Actuators, A 125 (2006) 148.
- 2 D. A. Krohn: Fiber Optic Sensors: Fundamentals and Applications (Instrument Society of America, Research Triangle Park, North Carolina, 1988).
- 3 M. M. Salour, G. Schoner, M. Kull and J. H. Bechtel: Electron. Lett. 21 (1985) 135.
- 4 K. Kyumn, S. Tai and T. Sawada: IEEE J. Quantum Electron. 4 (1982) 676.
- 5 T. J. De Lyon, J. A. Roth and D. H. Chow: Vac. Sci. Technol. B 15 (1997) 329.
- 6 K. Kyumn, S. Tai, T. Sawada and M. Nunoshita: IEEE J. Quantum Electron. 18 (1982) 676.
- 7 Y. Zhao, M. Rong and Y. B. Liao: IEEE Sens. J. 3 (2003) 400.
- 8 M. F. Sultan and M. J. O'Rourke: Proc. SPIE 2839 (1996) 191.
- 9 G. Gagliardi, M. Salza, P. Ferraro, E. Chehura, R. P. Tatam, T. K. Gangopadhyay, N. Ballard, D. Paz-Soldan, J. A. Barnes, H.-P. Loock, T.-Y. Lam, J. H. Chow and P. De Natale: Sensors 10 (2010) 1823
- 10 C. Francesco, P. Alfredo and S. Antonio: IEEE Sens. J. 1 (2003) 80.
- 11 Y. H. Hai and S. T. Uday: Laser Reflection Optical Fiber Sensor, US Patent No. 0135427 (2009).
- 12 C. Tanguy: J. Appl. Phys. 80 (1990) 4626.
- 13 J. F. Bradley, B. L. Douglas and J. M. Timothy: Proc. SPIE **6273** (2006) 62732J.
- 14 J. Jan, N. Bernhard and B. Pawel: J. Opt. Soc. Am. B 21 (2004) 729.
- 15 P. J. L. Herve and L. K. J. Vandamme: J. Appl. Phys. 77 (1995) 5476.
- 16 L. Min and L. L. Yu: Appl. Opt. 2 (2012) 231.
- 17 P. D. Li, N. G. Li and F. Yu: Nature Magazine 25 (2003) 280.