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Surface Treatment for GaN Substrate —Comparison of Chemical Mechanical Polishing and Inductively Coupled Plasma Dry Etching—

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A direct comparison of surface treatment methods for GaN substrates, namely, chemical mechanical polishing (CMP) with a colloidal silica slurry and inductively coupled plasma (ICP) dry etching with SiCl₄ gas, is presented, and their advantages and disadvantages are summarized. The subsurface damage is evaluated from the intensity of the cathodoluminescence (CL) emission spectrum and by CL imaging. Although the CMP-finished GaN substrate exhibits a perfect surface free of scratches and subsurface damage, the removal rate achieved is insufficiently high. On the other hand, ICP dry etching is seen to be able to remove only subsurface damage with a remarkably high removal rate but not remove the scratches induced by the mechanical process. In addition, the introduction of plasma-induced damage during ICP dry etching is suggested. Clear evidence of the introduction of plasma-induced damage, which is a network of point defects originating from the mechanical effects of dry etching such as ion bombardment, is shown in this study by demonstrating the ICP dry etching for a CMP-finished GaN substrate and by discussing the reasons for the degradation in CL intensity. On the basis of the experimental results, the current issues to be solved for CMP as well as ICP dry etching are summarized toward the development of a suitable surface treatment for GaN substrate for III-nitride epitaxy.

1. Introduction

Single-crystal bulk GaN substrates are one of the most promising candidates to replace sapphire substrates, which are commonly used for III-nitride devices such as light-emitting diodes (LEDs) and laser diodes (LDs), and to improve III-nitride device performance markedly by enabling homoepitaxial growth of III-nitride device films. Single crystals of bulk GaN can be grown by high-pressure solution growth (HPGS),⁽¹⁾

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hydride vapor phase epitaxy (HVPE),^(2,3) ammonothermal growth,⁽⁴⁾ and liquid phase epitaxy (LPE).⁽⁵⁾ After the growth of bulk crystals, the crystal undergoes a wafering process, including cutting, grinding, mechanical polishing, and chemical mechanical polishing (CMP). The surface produced by mechanical processes has a dense network of scratches and damage. However, to obtain high-performance thin-film devices on GaN substrate by homoepitaxy, it is essential to achieve a surface free of scratches and damage for the GaN substrate. Therefore, the final step of the wafering process, CMP, plays an extremely important role in the quality of subsequent homoepitaxial GaN films and related devices.⁽⁶⁾

Recently, we have reported for the first time a perfect surface of GaN free of scratches and subsurface damage by CMP with a colloidal silica slurry, which is the only report to the best of our knowledge dealing with the complete CMP for the GaN substrate.⁽⁷⁾ In the report, we confirmed the feasibility of CMP for the GaN substrate as the surface treatment for producing the surface with a complete absence of damage and scratches. However, the achieved removal rate of GaN by CMP was not sufficiently high to apply the production process as the Ga face of GaN is inert to almost all chemical solutions.⁽⁸⁾ Considering the insufficient development in the CMP for GaN substrate, dry etch is widely used as the final surface treatment for the GaN substrate as it is already commonly used for producing the mesa structure in nitride thin films in the device process of LEDs and LDs.^(9–11) Reactive ion etching (RIE), electron cyclotron resonance (ECR), and inductively coupled plasma (ICP) technology are used in this approach. The most important feature of plasma dry etching is the much faster etching rate of GaN than in the wet processes.⁽¹²⁻¹⁴⁾ However, in general, the plasma dry etching removes subsurface damage induced by the mechanical polishing but it does not remove the scratches since dry etching proceeds randomly without reference to a flat surface. Thus, the scratches produced by the mechanical processing before dry etching remain on the surface after dry etching. In addition to this, it has been reported that the plasma etching conditions for producing the mesa structure in nitride thin films in the device process strongly affect the degradation of the electrical performance of fabricated LEDs.^(8,15,16) This suggests that there is damage being introduced onto the surface of the GaN substrate by the plasma dry etching, which is the so-called "plasma-induced damage".

As described above, both CMP and dry etching seem to have advantages and disadvantages. However, there is no report dealing with their systematic comparison. Therefore, in this paper, we present for the first time a direct comparison of CMP and ICP dry etching surface treatment methods for GaN substrates. Both CMP with the colloidal silica slurry and ICP dry etching with SiCl₄ are applied to a GaN substrate pretreated by mechanical polishing with a diamond abrasive. The advantages and disadvantages of both CMP and ICP dry etching surface treatment methods are summarized, and a separate discussion of the factors affecting the surface roughness, damage removal, and damage introduced during each process is conducted to give insight into a suitable surface treatment of the GaN substrate for epitaxy. In addition, we will present for the first time as well a clear evidence of the introduction of plasma-induced damage by applying the ICP dry etching to the CMP-finished GaN substrate. The possible reasons for the generation of plasma-induced damage to the GaN substrate by plasma dry etching are also discussed in detail.

2. Experimental Procedure

2.1 Diamond polishing for GaN substrate as a preprocessing for final surface treatment

An as-lapped GaN substrate from a commercial source was used in this study. Prior to the final surface treatment with either CMP or dry etching, the GaN substrate was mechanically polished with a diamond abrasive in several steps using progressively smaller sized diamond abrasives. As the first step, a 2.0- μ m-diameter diamond abrasive (2.0 μ m diamond abrasive) was used to remove the initial surface roughness. The polishing with the 2.0 μ m diamond abrasive was followed by the second diamond polishing with a 0.5- μ m-diameter diamond abrasive (0.5 μ m diamond abrasive). Some of the GaN substrates polished with the 0.5 μ m diamond abrasive were subjected to the further polishing with a 0.25- μ m-diameter diamond abrasive (0.25 μ m diamond abrasive) before the final surface treatment. Detailed conditions of the diamond polishing processes are given in Table 1.

2.2 *CMP treatment for GaN substrate*

After the diamond polishing, CMP was employed in the GaN substrate. A tabletop polisher with a 300-mm-diameter platen was used for CMP process. The typical CMP conditions are described elsewhere.⁽⁷⁾ Among the several candidates of the slurry for CMP, colloidal silica is the most popular and used in the actual industries for CMP of silicon, glass, and sapphire substrate. Therefore, a commercially available colloidal silica was selected as a slurry for CMP of the GaN substrate. The removal rate of GaN by CMP was 17 nm/h under the typical CMP conditions.⁽⁷⁾

2.3 *ICP dry etching for GaN substrate*

Dry etching was also applied to the substrate pretreated by mechanical polishing with the diamond abrasive. Among the several dry-etching techniques, we employed ICP etching. This is because ICP etching can minimize damage while maintaining fast etching rates. In addition, ICP etching is generally believed to have several advantages in terms of scale-up for production, improved plasma uniformity over a wide area and low operation costs.⁽⁸⁾ A commercially available dry etcher, which is commonly used for the fabrication of the mesa structure for LEDs, was used for the dry etching of the GaN

		1st polishing	2nd polishing	3rd polishing
Abrasive size	(µm)	2	0.5	0.25
Applied pressure	(kg/cm ²)	0.1	0.1	0.1
Platen rotation	(min ⁻¹)	50	50	50
Platen size	(mm)	380	380	380
Platen material		Cu	Sn	Sn

Table 1 Conditions for preprocesses with diamond abrasive.

substrate. SiCl₄ gas was used as the etching gas. Two different etching rates were applied to etch the GaN substrate by changing the bias power: 185 and 685 nm/min, which is a typical range of the etching rate used for producing the mesa structure of LEDs and LDs.

2.4 Surface and subsurface evaluations after surface treatment

The surface roughness was evaluated by optical microscopy (OM) and atomic force microscopy (AFM). Generally, mechanical polishing with diamond abrasives generates networks of dislocations at or near the surface region of the substrate. The dislocations related to surface defects such as scratches can be evaluated by regular surface analysis such as by OM and AFM. For the subsurface dislocations, however, we need a different approach to visualize their existence. In this work, the removal of subsurface damage induced by mechanical polishing is evaluated from the cathodoluminescence (CL) intensity and also visually understood by CL imaging. As dislocation areas act as nonradiative recombination sites, dislocations appear as dark areas in the CL image, leading to a decrease in the CL intensity.⁽¹⁷⁾ Therefore, CL evaluation is one powerful method for understanding the damage existing beneath the surface of GaN substrates.⁽⁷⁾ The CL was excited by accelerated electrons with the energy of 5 kV, corresponding to the maximum penetration depth of 0.22 µm.⁽¹⁸⁾

3. Results and Discussion

3.1 *CMP treatment for GaN substrate*

The surface conditions after the mechanical polishing with the diamond abrasive as a preprocessing for the final surface treatment were evaluated by OM and AFM. The OM image of the GaN substrate mechanically polished with a 0.5 μ m diamond abrasive is shown in Fig. 1. AFM images of the GaN substrate mechanically polished with 0.5 or 0.25 μ m diamond abrasive are shown in Figs. 2(a) and 2(b), respectively. Numerous scratches made by the diamond abrasive are observed in the OM and AFM images. The



Fig. 1. OM image of GaN surface processed with a 0.5 µm diamond abrasive.



Fig. 2. AFM image of GaN surface processed with a (a) 0.5 or (b) 0.25μ m diamond abrasive.

surface roughnesses after the 0.5 and 0.25 µm diamond polishing were 1.5 and 0.9 nm, respectively. Thus, the smaller diamond abrasive produces a smoother GaN surface.

Then, CMP was conducted for the substrates preprocessed by diamond polishing. The removal of subsurface mechanical damage during CMP was evaluated by CL. Figures 3(a)-3(c) show the CL images of the GaN surface after diamond polishing with the 0.5 µm diamond abrasive, at an intermediate stage of CMP, and after CMP. Just after the diamond polishing, the CL image is dominated by black lines as shown in Fig. 3(a). The black lines correspond to the subsurface damage induced by the mechanical polishing as the damaged areas act as nonradiative recombination sites. It can be seen that the number of black lines decreases with increasing CMP process time. In the case where the GaN surface was preprocessed with the 0.5 µm diamond abrasive, 150 h of CMP was required to obtain a damage-free surface. As Fig. 3(c) shows no black line, it indicates that CMP achieves a complete removal of subsurface damage induced by the mechanical polishing. In addition, after 150 h of CMP, a hexagonal morphology that corresponds to the crystalline structure of GaN is clearly observed, as shown in Fig. 3(c).

In the case where the GaN surface was polished with the 0.25 μ m diamond abrasive, the required time for CMP was reduced from 150 to 105 h. The subsurface damage depths induced by the 0.5 and 0.25 μ m diamond abrasives can be estimated to be around 2.5 and 1.7 μ m, respectively, considering the required time for CMP and the removal rate. We note that there was no significant difference in the surface quality after CMP between the GaN substrate preprocessed with the 0.5 and 0.25 μ m diamond abrasives. Therefore, the size of the diamond abrasive simply contributes to the shortening of the CMP time by reducing the depth of subsurface damage induced by mechanical polishing.

AFM images after 150 h of CMP are shown in Fig. 4, exhibiting the scratch-free surface. A crystal-oriented surface morphology is clearly observed in Fig. 4(a). The surface roughnesses were 0.3 and 0.2 nm over 50×50 and $5 \times 5 \ \mu\text{m}^2$ areas, respectively. In the 5 \times 5 $\ \mu\text{m}^2$ area AFM image (Fig. 4(b)), we see crystal-oriented atomic step structures due to crystal misorientation. As a result, it is concluded that an atomically



Fig. 3. CL images of the GaN substrate (a) before, (b) at an intermediate stage of CMP (70 h of CMP), and (c) after CMP (150 h of CMP). Preprocessing of CMP is mechanical polishing with a 0.5 μ m diamond abrasive.



Fig. 4. AFM image of GaN surface after CMP over (a) 50×50 and (b) $5 \times 5 \ \mu\text{m}^2$ areas. Preprocessing of CMP is mechanical polishing with a 0.5 μ m diamond abrasive.

flat surface without subsurface damage is produced by CMP with colloidal silica slurry. However, the extremely low removal rate, 17 nm/h, is a serious issue for CMP of the GaN substrate, causing the necessity of over 100 h of CMP.

3.2 *ICP dry etching for GaN substrate*

As mentioned above, it was found that the thickness needed to remove the subsurface damage induced by mechanical polishing is around 2.5 μ m for the GaN substrate preprocessed with the 0.5 μ m diamond abrasive. Therefore, at least 2.5 μ m of the GaN substrate was etched from the surface by ICP dry etching using SiCl₄ with a 185 nm/ min etching rate. In the dry etching, the initial scratches produced by the mechanical

polishing were emphasized as seen in the comparison between Figs. 1 and 5(a), which are the OM images of the surface before and after ICP dry etching, respectively. Thus, it is indicated that reduction of the scratch width and depth as much as possible is necessary for the preprocessing of dry etching.

To investigate the effect of the smaller diamond abrasive for the preprocessing on the surface quality of the GaN substrate after dry etching, mechanical polishing with a 0.25 μ m diamond abrasive was applied after that with a 0.5 μ m diamond abrasive, and then, the substrate was subsequently processed by dry etching using SiCl₄ with a 185 nm/min etching rate. As the subsurface damage thickness that needed to be removed was 1.7 μ m in this case based on the CMP experiments, at least 1.7 μ m of the GaN substrate after the dry etching is shown in Fig. 5(b). By preprocessing with the 0.25 μ m diamond abrasive, much improved surface quality and less-damaged surface were achieved after the dry etching. The detailed surface roughness was evaluated by AFM as shown in Fig. 6. As compared with the surface before dry etching (Fig. 2(b)), the surface roughness was degraded from 0.9 to 1.9 nm. Therefore, it is suggested that the dry etching cannot produce an atomically flat surface.

Figure 7 shows the CL images of GaN after the dry etching. While visible scratches still remain on the surface after dry etching of the GaN substrate as seen in the surface observation by OM and AFM, it is found that dark lines corresponding to the mechanical damage induced by mechanical polishing were completely removed by ICP dry etching regardless of the diamond abrasive size used in the preprocessing (see Fig. 3 for reference). However, as seen in the comparison between Figs. 7(a) and 7(b), we see a large difference in the clearness and intensity of the CL emission images between the surfaces finished by ICP dry etching with 0.5 μ m diamond abrasive preprocessing and that with 0.25 μ m diamond abrasive preprocessing. The depth of the damaged layer produced by mechanical polishing is known from the CMP experiments, and we



Fig. 5. OM image of GaN surface after dry etching. Preprocessing of dry etching was mechanical polishing with a (a) 0.5 or (b) $0.25 \mu m$ diamond abrasive.



Ra = 1.9 nm

Fig. 6. AFM image of GaN surface after dry etching. Preprocessing of dry etching was mechanical polishing with a 0.25 μ m diamond abrasive.



Fig. 7. CL images of the GaN substrate after dry etching. Preprocessing of dry etching is mechanical polishing with a (a) 0.5 or (b) $0.25 \,\mu$ m diamond abrasive.

removed it completely by ICP dry etching. Therefore, the lower CL intensity for the dryetched GaN substrate suggests that a plasma-induced damage is introduced during the ICP dry etching. A longer plasma irradiation time seems to lead to an accumulation of the plasma-induced damage.

As a result, it is confirmed that subsurface damage removal induced by mechanical polishing can be achieved by ICP dry etching with a remarkably high etching rate. However, since the dry etching proceeds randomly without reference to a flat surface, the surface scratches produced by mechanical polishing are not removed by the dry

etching. Thus, it is thought to be important for the pretreatment for dry etching to reduce the depth of the scratches as much as possible. It was also suggested that the ICP dry etching newly introduced subsurface damage, namely, plasma-induced damage.

3.3 Evidence of introduction of plasma-induced damage by ICP dry etching

By comparing the two surface treatments, CMP and ICP dry etching, their advantages and disadvantages were revealed. However, the discussion on the subsurface damage and plasma-induced damage, and their relationship with CL intensity between the treatments has not been sufficiently done yet. Therefore, to directly discuss them, the CMP-finished GaN substrate was etched by ICP dry etching using SiCl₄ with two different etching rates: 185 and 685 nm/min. The etched depth was 0.5 μ m for both etching rates.

Figure 8 shows the AFM image after dry etching at a rate of 185 nm/min. The crystal-oriented surface features observed after CMP (Fig. 4) disappeared after dry etching. The substrate threading dislocations are observed to have been heavily etched and holes were formed on the surface. The surface roughness increased after dry etching from 0.3 to 0.9 nm. Figures 9(a) and 9(b) show the CL images after ICP dry etching at the rates of 185 and 685 nm/min, respectively. The clarity of the CL image diminishes after the dry etching (see Fig. 3(c) for reference CL image of CMP-finished GaN substrate). This is also detailed in Fig. 10, showing the CL spectrum from these samples and a typical CMP-finished GaN substrate as a reference. The CL intensity is seen to decrease with increasing ICP etching rate. These results, therefore, clearly suggest that ICP dry etching introduces subsurface damage, namely, this is a clear evidence of plasma-induced damage to the GaN substrate. It can also be concluded that a higher ICP dry etching rate leads to a more serious degradation of the GaN substrate surface quality.

The possible reasons for the degradation of the CL intensity and its relationship with the plasma-induced damage are worth discussing. There are some related reports on the



Ra = 0.9 nm

Fig. 8 AFM image of GaN surface dry-etched at a 185 nm/min etch rate. Image size is $50 \times 50 \ \mu m^2$.



Fig. 9. CL image of GaN substrate dry-etched at a (a) 185 or (b) 685 nm/min etch rate. Preprocessing of dry etching is CMP.



Fig. 10. CL spectrum from GaN surface after dry etching at (a) 185 and (b) 685 nm/min etch rates. Preprocessing of dry etching is CMP. The CL spectrum from as-CMP GaN surface is also shown in (c) as a reference.

deterioration of the photoluminescence (PL) intensity of GaN thin films after dry etching in the mesa structure production for LEDs, and the following three possible reasons have been suggested: (1) formation of Ga–O bonds at the GaN surface,^(16,19) (2) adsorption of Cl atoms on and near the surface,^(15,20) and (3) destruction of the GaN crystal surface.⁽²¹⁾ To understand the observed deterioration in the CL intensity due to ICP dry etching, these three factors should be discussed.

- (1) Formation of Ga–O bonds at the GaN surface: Han *et al.*⁽¹⁶⁾ reported evidence of Ga –O formation on the Cl₂/Ar ICP-etched GaN thin film surface. The oxidation may occur when the GaN film surface was exposed to the air environment after ICP dry etching. It has been reported that oxygen bonded to GaN serves as a nonradiative recombination site.⁽¹⁹⁾ On the other hand, it has also been reported that GaN is polished by the surface oxidation mechanism of forming Ga₂O₃ followed by the dissolution of Ga₂O₃ into a chemical solution.^(22–24) Therefore, the CMP-finished GaN surface already forms Ga₂O₃.^(25,26) Considering that the best CL intensity was obtained from the GaN surface finished by CMP, the formation of Ga–O bonds at the GaN surface by ICP dry etching is not considered to be a reason for the degradation of the CL intensity.
- (2) Adsorption of Cl atoms on and near the surface: As Cl shows strong electronegativity, it may affect the electrical conditions of the surface atoms and thus affect electron behavior during CL measurements. Therefore, measurement of the Cl contamination on and near the surface by total X-ray reflection fluorescence (TXRF) and removal of the surface-adsorbed Cl by cleaning with a wet acid solution (a mixture of H₂SO₄ and H₂O₂) for 10 min at 100°C were conducted using the GaN substrate finished with CMP and subsequent ICP dry etching. Figure 11 shows the number of surface Cl atoms measured by TXRF. There is a difference of two orders of magnitude in the number of adsorbed Cl atoms between the CMP-finished and dry-etched GaN. After cleaning, some adsorbed Cl atoms are removed, and the number of Cl atoms drops to the same level as that of the CMP-finished GaN substrate. Figure 12 shows



Fig. 11. Comparison of the number of chlorine atoms measured by TXRF for surface of (a) as-dry etched, (b) dry etched and then cleaned with wet acid, and (c) as-CMP-finished GaN substrate.



Fig. 12. CL spectrum from surface of (a) as-dry etched, (b) dry etched and then cleaned with wet acid, and (c) as-CMP-finished GaN substrate.

the CL spectra of the GaN substrate treated by ICP dry etching before and after cleaning together with the CMP-finished surface for reference. The CL intensity increased slightly after cleaning. However, there is still a large difference between the CMP-finished and cleaned GaN surfaces. Therefore, Cl adsorption on and near the GaN surface is not the main cause of the deterioration in the CL intensity.

(3) Destruction of the GaN crystal surface: This is likely to be the most reasonable explanation for the lower CL intensity since reasons (1) and (2) have been rejected. Jeong *et al.*⁽²⁷⁾ reported that the plasma-induced damage on the N face of GaN can be removed by KOH etching with an etch depth of ~500 nm. They also reported that the etching rate of the N face of GaN by KOH etching is markedly affected by the previous ICP etching conditions. These results may indicate that the plasma-induced damage is created inside the crystal as subsurface damaged layers. In addition, Waki *et al.*⁽²⁸⁾ have reported the reaction scheme for CI-based ICP dry etching, and the etching reaction is reported to proceed with the following steps: neutral CI adsorption, reaction of CI with GaN to form etch products, and ion bombardment in ICP dry etching is considered to mechanically affect the GaN surface and to create nonradiative recombination centers as, presumably, a network of point defects. Consequently, the related CL intensity degradation was observed for the GaN substrate after ICP dry etching.

3.4 Summary

Before providing the conclusions, here, we summarize the advantages, disadvantages, and effect of preprocessing on the surface quality for CMP and ICP dry etching.

- (1) Advantages of CMP: CMP produces an atomically flat surface and complete absence of subsurface damage simultaneously.
- (2) Disadvantage of CMP: the removal rate is insufficiently high under typical CMP conditions.
- (3) Effect of preprocessing for CMP: the use of mechanical polishing with the smaller diamond abrasive contributes to the reduction of the required CMP time for producing the complete damage-free surface but does not affect the CMP surface quality.
- (4) Advantage of ICP dry etching: the removal of subsurface damage induced by mechanical polishing is achieved with a remarkably high etching rate.
- (5) Disadvantages of ICP dry etching: no planarization effect can be obtained (scratches remain on the surface after ICP dry etching), and introduction of a network of point defects as plasma-induced damage occurs.
- (6) Effect of preprocessing for ICP dry etching: producing the smoother surface and shallower subsurface damage by mechanical polishing with the smaller diamond abrasive contribute to the better surface roughness and reduced plasma-induced damage.

Finally, as future tasks, CMP requires the marked improvement in the removal rate. On the other hand, ICP dry etching requires a suitable preprocessing to minimize the surface roughness and reduced introduction of plasma-induced damage to suppress the network of point defects. By resolving the issues revealed in this study, surface finishing technique will be established for GaN substrate manufacturing in mass-production scale, which will lead to an acceleration of the use of the GaN substrate for LEDs and LDs, and the realization of next-generation high-frequency, high-power devices with GaN substrate.

4. Conclusions

The first direct comparison of CMP and dry etching surface treatment methods for GaN substrates was presented, and the advantages and disadvantages of the surface treatment for GaN substrate are experimentally compared to understand the current issues for these techniques and to provide insight for the development of a suitable surface treatment for the GaN substrate. CMP finishing of the GaN substrate exhibits a perfect surface free of scratches and damage. However, the extremely low removal rate in CMP is found to be a critical issue. On the other hand, ICP dry etching exhibits a remarkably high removal rate and removal of the subsurface damage induced by mechanical polishing. However, ICP etching does not remove the surface scratches produced by the mechanical process. In addition, plasma-induced damage as a result of the ICP dry etching is observed clearly in the deterioration of the CL intensity after ICP dry etching of the CMP-finished GaN substrate. The deterioration of the CL intensity is considered to be caused by the creation of nonradiative recombination sites that are presumably a network of point defects originating from the mechanical effects of dry etching such as ion bombardment. Finally, the current issues to be resolved for CMP and ICP dry etching have been understood clearly toward the development of a suitable surface treatment for GaN substrate. These are (i) a marked improvement in the removal rate of CMP, (ii) a suitable preprocessing for ICP dry etching, and (iii) reduced introduction of plasma-induced damage.

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