

A MEMS Accelerometer for Sub-mG Sensing

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In this paper, we present a highly sensitive micro-electromechanical system (MEMS) accelerometer for sub-mG sensing resolution, where the thermomechanical noise (i.e., Brownian noise, B_N) being inversely proportional to a proof mass has to be below $1 \mu\text{G}/\sqrt{\text{Hz}}$ (gravity acceleration $G = 9.8 \text{ m/s}^2$). To increase the proof mass, we propose the use of multiple-layered metal developed by Au electroplating. We then show an approach to design the spring constant for the MEMS accelerometer. A multilayer metal structure is used for serpentine flexures to suspend the high-density proof mass, which also enables us to obtain a high degree of freedom for the spring constant design without compromising the performance of the MEMS accelerometer. A proof-of-concept device has been fabricated, and the measured characteristics are consistent with the design values. The B_N of the developed device is experimentally evaluated to be $22 \text{ nG}/\sqrt{\text{Hz}}$, which is one or more orders of magnitude lower than those of conventional MEMS accelerometers with the same capacitance sensitivity. The evaluation results confirm that the proposed device has potential for sub-mG sensing.

1. Introduction

Micro-electromechanical system (MEMS) accelerometers have become key devices for inertial sensing technology in a variety of applications.^(1,2) The sensing resolution of MEMS accelerometers for commercial use is commonly designed to sense more than 1 mG (gravity acceleration $G = 9.8 \text{ m/s}^2$),^(3,4) and the resolution has to be further improved for future potential applications such as space applications, seismometry, and inertial navigation.^(5,6) To realize high-resolution acceleration sensing, it is necessary to reduce the noise in the MEMS accelerometer. Thermomechanical noise (i.e., Brownian noise, B_N) is one of the dominant noise sources in MEMS accelerometers.⁽⁷⁻⁹⁾ Conventionally, large proof masses made of silicon were used to reduce B_N , since B_N is inversely proportional to the proof mass.⁽⁷⁻⁹⁾ Such methods need bulk-micromachining and/or wafer bonding techniques⁽¹⁰⁻¹⁸⁾ and result in large sensor modules.

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Thus far, the B_N 's of surface micromachined accelerometers are higher than $10 \mu\text{G}/\sqrt{\text{Hz}}$,^(19–21) and B_N below $1 \mu\text{G}/\sqrt{\text{Hz}}$ is only shown by bulk micromachined accelerometers for micro-G resolution.^(8,9,14,15) In our previous works, we have proposed high-resolution MEMS accelerometers with a high-density Au proof mass^(22,23) developed by Au electroplating.⁽²⁴⁾

In this paper, we present a Au proof-mass MEMS accelerometer for sub-mG sensing. Multilayer metal structures are newly employed for both the proof mass and the spring in the MEMS accelerometer, which contribute to the decrease in B_N . Analysis and experimental results confirm the feasibility of the proposed approach. In the following sections, we first show a design concept of the device and design methods for the proof mass and spring structures. Next, a device fabrication process using multilayer metal technology is described. Finally, we show the experimental evaluation results and the performance comparison with conventional devices.

2. Device Design and Fabrication

In this section, we describe the design concept of the proposed MEMS accelerometer and materials used. Then, design methods for the proof mass and spring structures are shown with analysis results. Lastly, we present the device fabrication process.

2.1 Design concept

Figure 1 shows the design concept of a single-axis capacitive^(19–21) MEMS accelerometer with a Au proof mass. For a high-resolution capacitive MEMS accelerometer, both the mechanical and electrical noises have to be minimized. The major part of mechanical noise is dominated by B_N , which is given by

$$B_N = \frac{\sqrt{4k_B T b}}{m}, \quad (1)$$

where k_B , T , b , and m are the Boltzmann constant (1.38×10^{-23} J/K), absolute temperature, viscous damping coefficient, and proof mass of an accelerometer, respectively.⁽¹⁹⁾ As shown in Eq. (1), B_N is inversely proportional to the proof mass. MEMS capacitive accelerometers conventionally utilize Si mechanical structures and employ a large Si proof mass when a low B_N is required. We previously proposed an alternative approach^(22,23) to reducing B_N in a MEMS accelerometer, where we used a Au proof mass developed by a multilayer metal technology.⁽²⁴⁾ The density of Au ($19.3 \times 10^3 \text{ kg/m}^3$ at 298 K)⁽²⁵⁾ is nearly an order of magnitude higher than that of Si ($2.33 \times 10^3 \text{ kg/m}^3$ at 298 K),⁽²⁵⁾ and thus we can achieve B_N lower than that of a Si proof mass of the same dimensions.

For sub-mG ($<10^{-3}$ G) sensing, the target B_N of this work was determined to be below $50 \text{ nG}/\sqrt{\text{Hz}}$,⁽²³⁾ where the frequency band is set to be 10 Hz.⁽²³⁾ The total noise of a capacitive accelerometer consists of B_N and electrical noise.⁽²⁶⁾ In this study, we assume that the electrical noise is negligibly small, which can be achieved by considering the sensing circuit technology⁽²⁷⁾ and large sensitivity, typically on the order of several pF/G.

Figure 2 shows the analysis results of B_N as a function of proof-mass size, where T and b are set to be 298 K and 1.85×10^{-5} N·s/m, respectively. The thickness of the Si proof mass is set to be 10 μm , which is a typical value of conventional surface-micromachined MEMS accelerometers.^(28–30) Owing to its high density, the Au proof mass has a lower B_N than a Si proof mass. Thus, we have developed Au proof mass structures with a thickness of more than 12 μm .⁽²³⁾ To achieve B_N below $50 \text{ nG}/\sqrt{\text{Hz}}$, the thickness of the Au proof mass has to be increased. The proof mass of a MEMS accelerometer developed by the multilayer metal technology has release holes for sacrificial etching; thus, a 4-mm-square proof mass with a thickness of 10 μm is insufficient to achieve a noise level below $50 \text{ nG}/\sqrt{\text{Hz}}$. In this work, we designed a multilayer Au proof mass with a total thickness of 20 μm . As the thickness of a single Au layer in the multilayer technology was smaller than 20 μm , we proposed to utilize multiple Au layers for the proof mass. The proof-mass structure of 20 μm thickness can be achieved by using two Au layers in the multilayer metal technology. In this design, we assume that the proof mass is a perforated plate with equally spaced release holes, and the viscous damping coefficient b can be expressed by⁽³¹⁾

$$b = 0.427N\mu \frac{L^4}{d^3}, \quad (2)$$

$$L = \sqrt{p^2 - a^2}, \quad (3)$$

where N , μ , d , and L are the number of damping holes, the viscosity of the surrounding gas, the air gap, and the effective proof-mass length with the release hole pitch p and size a , respectively. We use 1.8×10^{-5} N·s/m² for the viscosity of air⁽³²⁾, and N , d , p , and a are designed to be 15376, 5.92 μm , 16 μm , and 8.7 μm , respectively. As a result, b is estimated to be 1.85×10^{-5} N·s/m.

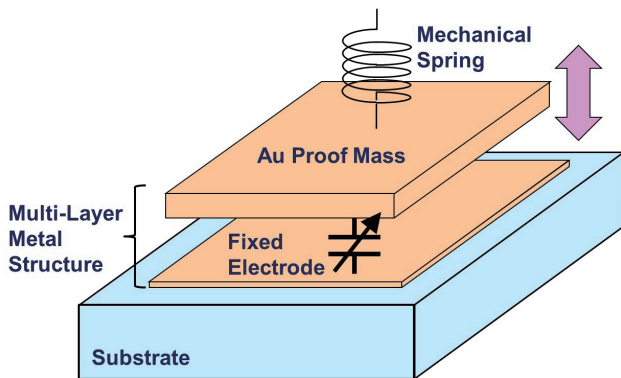


Fig. 1. (Color online) Schematic of a high-density Au proof-mass MEMS capacitive accelerometer.

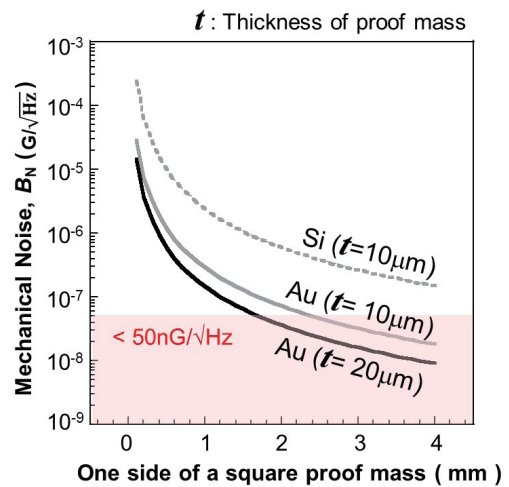


Fig. 2. (Color online) Mechanical noise analysis results.

2.2 Spring structure

The Au proof mass can become one order of magnitude higher than the Si proof mass as shown in Fig. 3; thus, the spring constant of micromechanical flexure has to be larger than those of conventional Si types. Figure 4(a) shows an analytical model of the offset displacement of the proof mass at the input of the gravitational acceleration of 1 G , and the analysis results of the offset displacement d of a 4-mm-square proof mass are shown in Fig. 4(b). In a practical manner, the offset displacement of the Au proof mass has to be designed to be as small as that of a silicon proof mass. The analysis results indicate that the spring constant used for the Au proof mass should be nearly one order of magnitude higher than that of silicon MEMS accelerometers.

Serpentine spring structures⁽³³⁾ would be useful for multiaxis acceleration sensing with a single proof mass, because the flexibility of tuning a 3-axis spring constant is higher than that of simple structures such as cantilever springs. Figure 5(a) shows an analytical model of a serpentine spring structure. Calculated Z-axis spring constants of serpentine flexures made of Au are shown in Fig. 5(b). Table 1 shows the analysis formula of the serpentine flexure, where we assume that the model is a guided-end spring with a concentrated load as the end and that L_c is equal to L_a .⁽³³⁾ In Fig. 5(b), we used typical dimensions of the MEMS accelerometer fabricated by the multilayer metal technology;⁽³⁴⁾ the parameters L_a , L_b , and w were set to be 200, 10, and 6 μm , respectively. Young's modulus and Poisson's ratio of Au used in the analysis were 78 GPa and 0.44, respectively.⁽³⁵⁾ The spring constants of 3- μm -thick serpentine flexures are insufficient to suspend a Au proof mass with a practical offset displacement up to 1 μm , as shown in Fig. 4(b). For a higher stiffness in the Z-axis direction, we designed a serpentine flexure of 15 μm thickness and proposed to use the third and fourth Au layers in the multilayer metal technology. Using multiple Au layers, which have been newly introduced in this work, enables us to increase the degree of freedom of MEMS design in the multilayer metal technology. Reducing flexure lengths, such as L_a and L_b , results in a shorter tuning range for stiffness. For instance, in order to achieve the Z-axis spring constant of a 15- μm -thick serpentine flexure, the L_a of a 3- μm -thick serpentine flexure has to be smaller than w , and such design cannot be allowed.

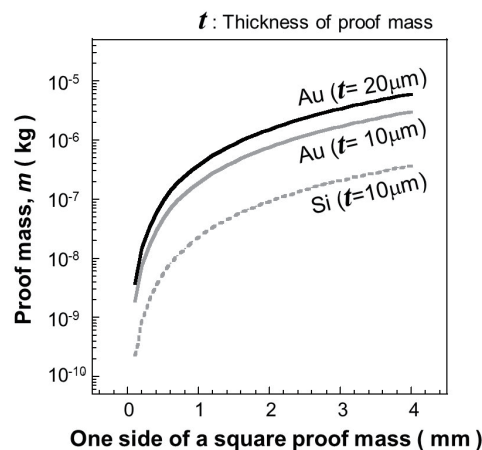


Fig. 3. Proof mass analysis results.

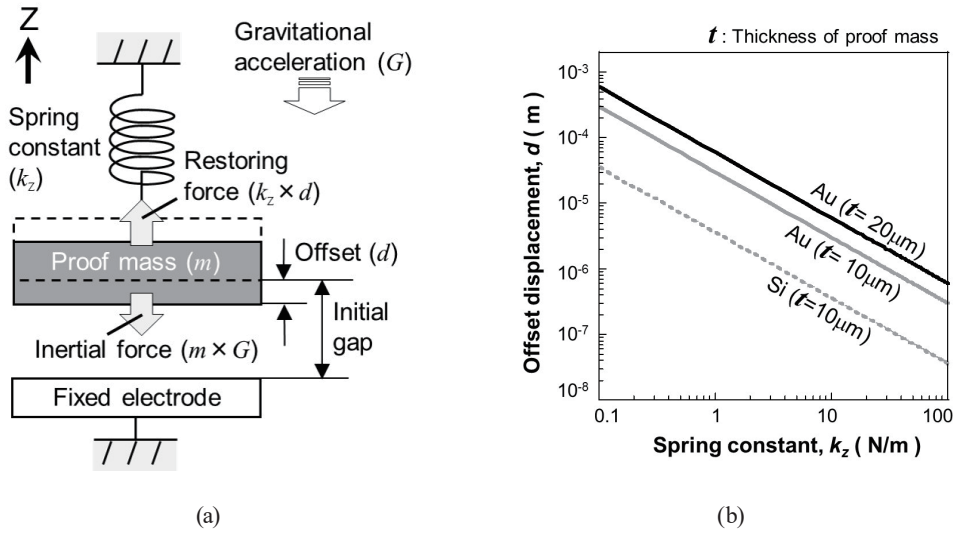


Fig. 4. Proof-mass offset with different spring constant. (a) Analytical model and (b) analysis results.

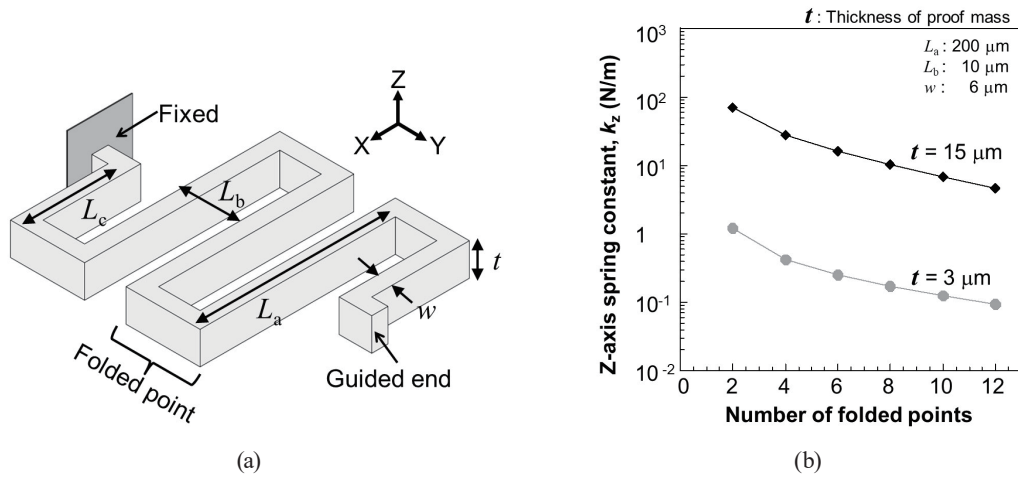


Fig. 5. Spring constant of serpentine structure. (a) Analytical model and (b) analysis results.

Table 1

Analysis formula of serpentine flexure.

Axis	Spring constant of serpentine flexure
Z	$k_z = 12 \frac{S_{EL_b} S_{EL_a} S_{GL_b} S_{GL_a}}{S_{EL_b} S_{GL_b} L_b^2 (S_{GL_b} L_b + S_{EL_b} L_a) n^3 - 3 S_{EL_b} S_{EL_a} S_{GL_b} L_b^2 L_a n^2 + S_{EL_b} L_a (2 S_{EL_b} S_{GL_b} L_b^2 + 3 S_{EL_b} S_{GL_b} L_b L_a + S_{GL_b} S_{GL_b} L_a^2) n - S_{EL_b} S_{GL_b} S_{GL_b} L_a^3}$ <p>where $S_{EL_b} = EI_{x,L_b}$, $S_{EL_a} = EI_{x,L_a}$, $S_{GL_b} = GJ_{x,L_b}$, $S_{GL_a} = GJ_{x,L_a}$, $J = \frac{1}{3} t^3 w \left(1 - \frac{192}{\pi^5} \frac{t}{w} \sum_{i=1, \text{odd}}^{\infty} \frac{1}{i^5} \tanh\left(\frac{i\pi w}{2t}\right) \right)$</p>
*Concentrated load and guided-end model, n : even, E : Young's modulus, $G = E/2(1+\nu)$, ν : Poisson's ratio, $I_{z,L_a} = I_{z,L_b} = tw^3/12$, $I_{x,L_a} = I_{x,L_b} = t^3w/12$, L_a , L_b , w , and t are shown in Fig. 5.	

2.3 Device fabrication

Figure 6 shows a schematic image of the proposed single-axis MEMS capacitive accelerometer. The device is realized by the multilayer technology based on electroplating, which has been reported elsewhere.⁽³⁶⁾ As mentioned in the device design methods, we utilize the third (M3) and fourth (M4) layers for the spring structure, and the M4 and fifth (M5) layers for the proof mass. The stoppers are immobilized structures and used to prevent the self-destruction of the movable parts at the input of excessive acceleration. When an excess acceleration is applied to the device, the proof mass collides with either the stopper or the bottom fixed electrode, protecting the spring structures from stretching out of the elastic deformation range. Figure 7 shows the device fabrication process flow. Firstly, Ti/Au seed layers were deposited by evaporation on a silicon wafer with a thermally formed SiO₂ layer, as shown in Fig. 7(a). A Au electroplating process was then used to increase the thickness of the first Au layer (M1). For sacrificial layer fabrication, photosensitive polyimide was spin-coated and annealed at a temperature of 310 °C. A SiO₂ layer of 1 μm thickness was deposited by sputtering [Fig. 7(b)]. With the same Au patterning as for the M1 layer, we made another five Au layers (M2–M6), as illustrated in Fig. 7(c). Finally, all the sacrificial layers made of photosensitive polyimide were removed by O₂ plasma dry etching [Fig. 7 (d)].

Figure 8(a) shows a chip view of the developed MEMS accelerometer. A Au proof mass was fabricated on a silicon substrate with a footprint of 4 × 4 mm². The device was implemented in a ceramic package and wire-bonded to have electrical connections with external instruments for experimental evaluation. The SEM image of the proof mass is shown in Fig. 8(b). The Au proof-mass structure of 22 μm thickness was successfully developed by employing the M4 and M5 layers. To minimize the effect of the metal warpage, the proof mass was segmented into sub-blocks that were cross-linked by the M6 layer. Through-holes were made to enhance the

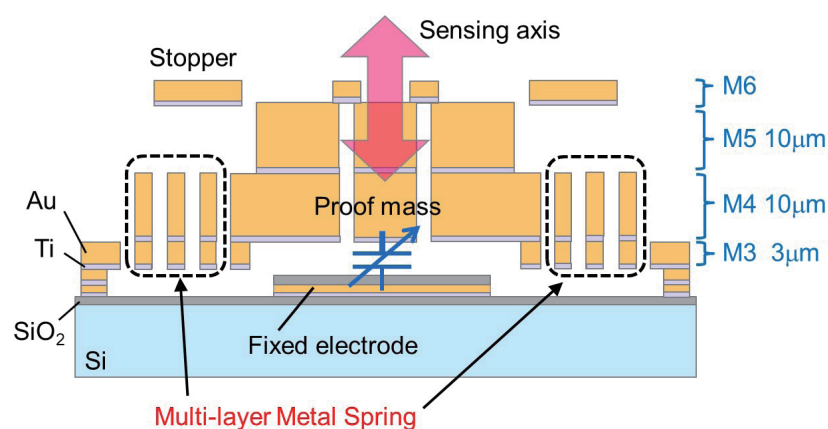


Fig. 6. (Color online) Schematic cross section of multilayer metal spring structures in a Au proof-mass MEMS capacitive accelerometer.

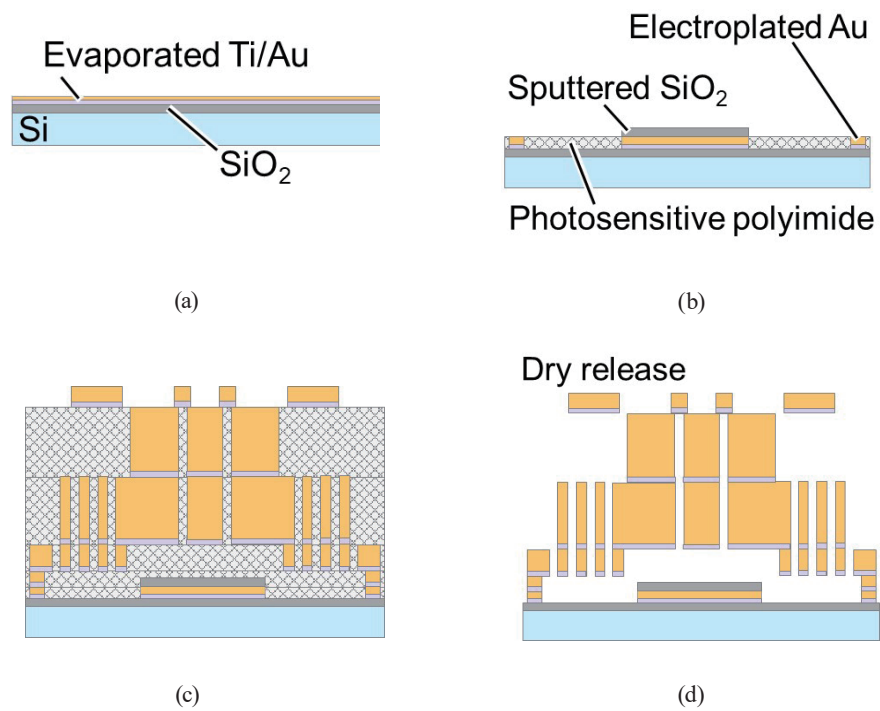


Fig. 7. (Color online) Process flow. (a) Seed layer deposition, (b) M1 and SiO₂ patterning, (c) M2–M6 patterning, and (d) sacrificial layer etching.

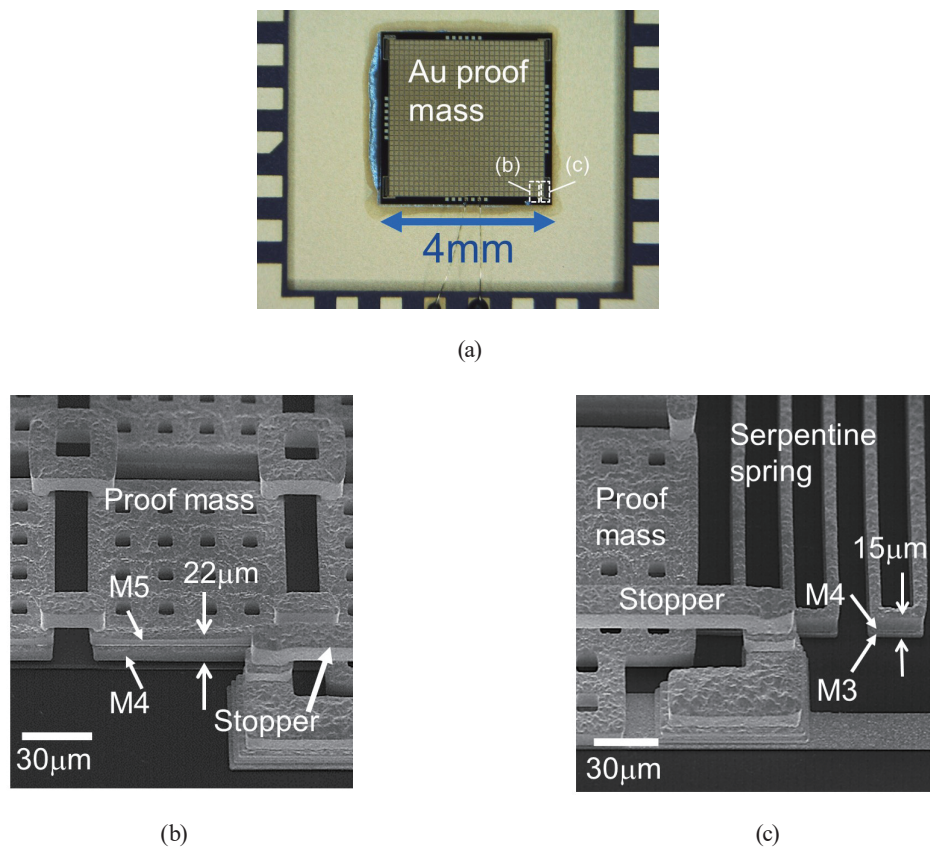


Fig. 8. (Color online) Fabricated device. (a) Chip view, (b) proof mass, and (c) spring structure.

sacrificial layer etching underneath the proof mass. Figure 8(c) shows the SEM image of the serpentine spring structure made of M3 and M4 layers. Stopper structures were made of the M6 layer and set above the proof mass. The serpentine springs and stoppers were placed at each corner of the proof mass.

3. Experimental Results and Discussion

3.1 Acceleration responses

We measured the capacitance between the proof mass and the fixed electrode when Z-axis acceleration was applied to the device as shown in Fig. 9. Figure 9(a) shows the experimental setup, where the packaged MEMS device was set on a custom-designed printed circuit board (PCB) on a vibration exciter (WaveMaker05, Asahi Seisakusho) with a minimum input-acceleration step of 0.01 G . A semiconductor device analyzer (B1500A, Agilent Tech., Inc.) was used to supply a DC bias voltage of 0.5 V and measure the capacitance change with a ± 0.1 V sinusoidal voltage at a frequency of 300 kHz. Figure 9(b) shows the measured capacitance as a function of input acceleration at a frequency of 49.9 Hz. The sensitivity was experimentally obtained to be 3.3 pF/G, which showed the potential of sub-mG sensing with capacitance-to-voltage converter circuits.⁽²⁷⁾

3.2 Frequency characteristics

For the evaluation of mechanical characteristics and B_N , we measured the frequency responses of the fabricated MEMS device. Figure 10 shows the capacitance and phase between the proof mass and the fixed electrode as a function of signal frequency. Figure 10(a) shows the experimental setup with an LCR meter (IM3533-01, HIOKI E.E. Corp.). As shown in Fig.

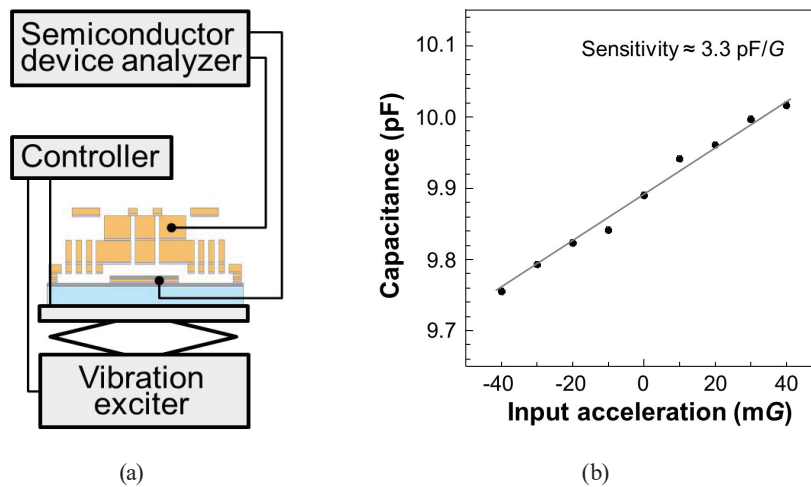


Fig. 9. (Color online) Measured capacitance as a function of input acceleration. (a) Experimental setup and (b) measurement results.

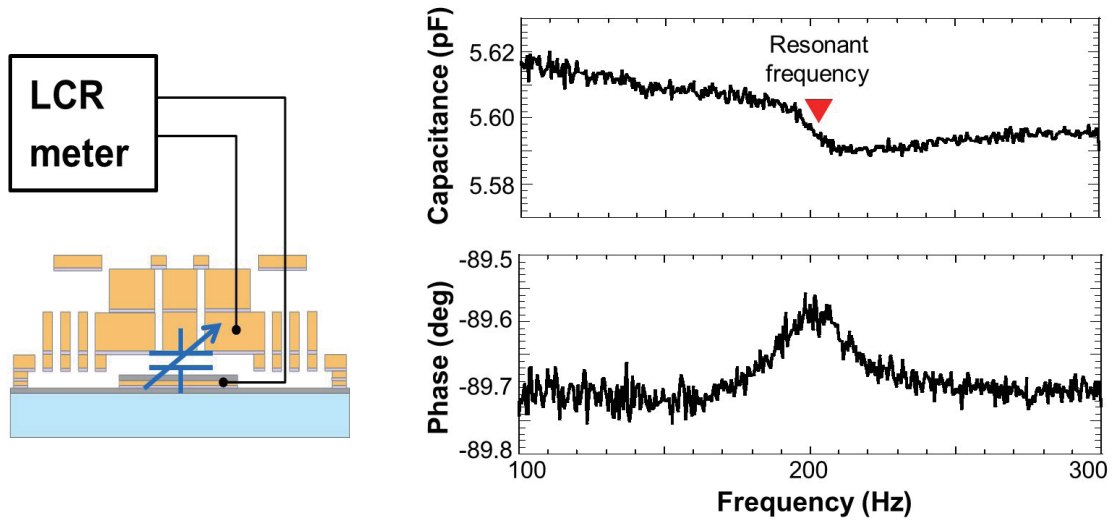


Fig. 10. (Color online) Measured capacitance and phase as a function of frequency. (a) Experimental setup and (b) measurement results.

10(b), the resonant frequency of the device was found to be 202 Hz with a DC bias voltage of 0.5 V. The actual proof-mass size was measured by an SEM. The difference between the designed and measured spring constants could be made by process variation that affects the dimension of serpentine spring structures. To evaluate the B_N of the device, the following relationship⁽²³⁾ was used:

$$B_N = \sqrt{\frac{4k_B T \omega_r}{mQ}}, \quad (4)$$

where ω_r and Q are the resonant angular frequency and quality factor, respectively. The designed Q is expressed as⁽³²⁾

$$Q = \frac{m\omega_{res}}{b}, \quad (5)$$

where ω_{res} is the resonant angular frequency. In the device design, the viscous damping coefficient b of 1.85×10^{-5} N·s/m is used, as mentioned in Sect. 2.1. Table 2 shows a summary of the designed and measured characteristics of the device, and the actual B_N was obtained to be 22 nG/ $\sqrt{\text{Hz}}$. The measured resonant frequency, spring constant, and quality factor are slightly lower than the designed values. The inconsistency could be caused by the difference between the designed and actual structure dimensions, and also by the warpage of the metal structures. Further investigation of these factors will be performed in our future works. Figure 11 shows a comparison of B_N versus capacitance sensitivity with conventional MEMS accelerometers. Owing to the high density of Au, the B_N achieved in this work was more than an order of magnitude lower than those of conventional devices when compared with the same sensitivity performance.

Table 2
Summary of device characteristics.

Parameter	Designed value	Measured value	Unit
Proof mass	3.28×10^{-6}	3.62×10^{-6}	kg
Z-axis resonant frequency	260	202	Hz
Z-axis spring constant	8.7	5.8	N/m
Quality factor	289	131	
BN	17	22	$\text{nG}/\sqrt{\text{Hz}}$

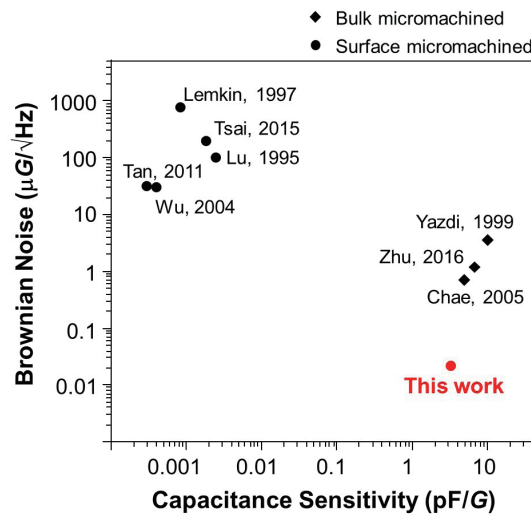


Fig. 11. (Color online) Comparison of BN versus capacitance sensitivity.^(10,11,19–21,37–39)

4. Conclusions

We proposed and demonstrated a Au proof-mass MEMS accelerometer for sub-mG sensing. In our design method, multilayer metal structures were used for both proof mass and spring for the first time. The multilayer structures contribute to the decrease in B_N without compromising the sensor performance and footprint. The measured characteristics of the developed MEMS devices were consistent with the designed values, demonstrating the feasibility of our approach. The experimentally obtained B_N was found to be $22 \text{ nG}/\sqrt{\text{Hz}}$. The B_N of the developed sensor was more than one order of magnitude lower than those of conventional MEMS accelerometers with the same capacitance sensitivity. The evaluation results confirmed that the proposed MEMS device has potential for sub-mG sensing.

Acknowledgments

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